Annex 6-E Acoustic Assessment Technical Supporting Document Denison Mines – Wheeler River Project

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APPENDICES

Appendix A: Assessment Scenarios and Sound Level Data

1.0 INTRODUCTION

This technical report is supplementary to the discussion of the noise impact assessment provided in the main body of the Environmental Impact Statement (EIS) report (Section 6 – Atmospheric and Acoustic Environment). The purpose of this supplemental report is to provide additional technical background details on the assessment methodology, assessment scenarios, source identification and characterization, predictive modelling, and modelling outputs.

2.0 ASSESSMENT SCENARIOS

The Wheeler River Project (the Project) will be completed in four phases: construction, operation, decommissioning, and post-decommissioning. As the nature of operations in each phase differs, the noise assessment scenarios were developed with consideration to each of these phases so as to effectively bound the potential noise effects of the Project over its entire life cycle. Based on the description of associated activities the Construction and Operations scenarios have the greatest potential to influence off-site sound levels. The Decommissioning phase is expected to be similar in nature to the construction phase; however, will not involve as much equipment and truck traffic, there will be no drilling, and the freeze plant will no longer be operating. As such, the Construction stage is expected to bound (i.e., have greater potential for impacts relative to) the Decommissioning stage. The Post-decommissioning phase will involve the least amount of activity of all of the phases, as it primarily involves monitoring conditions at the site over time. As such, the assessment of the Site Construction and Operations phases is expected to fully bound the noise impacts from the Project. These scenarios are discussed in further detail in the following sections.

2.1 CONSTRUCTION SCENARIO

The Construction scenario was based on the activities associated with the first year of construction, which, as planned, involves the most equipment operating on the site during the three-year construction phase. During this first year it is projected that there will be surface facilities construction occurring simultaneously with wellfield drill mobilizations, drilling of freeze holes and ISR wells, and partial operation of the freeze plant. The maximum scenario that was modelled includes the following general activities:

- Surface construction occurring at the ISR Plant location,
- Operation of a concrete batch plant and crusher,
- Freeze plant constructed and operating (partial operation, 2 of 6 units operating),
- Drill rigs operating in the wellfield (ISR wells),
- Deposit of drill waste in the clean waste pile,
- Power supplied by two (2) 1.1 MW generator sets, operating near the Freeze Plant and ISR plant,
- Power supplied by two (2) 450 kW generator sets, operating near the accommodations centre and the operations centre,
- Various vehicle movements (fuel, food, supplies for construction and wellfield development, on-site traffic), and
- Air traffic associated with construction crew changes.

The detailed source inventory for the Construction scenario, and approach to the characterization of each source are discussed in Section 3.0.

2.2 **OPERATIONS SCENARIO**

The Operations scenario was based on activities being completed in the late stages of the operations phase, with work being completed in Phase 5 of the deposit. Well drilling would continue, and the freeze plant was assumed to be operating at maximum capacity (all 6 skids running). While the site will be powered from the provincial grid at this stage, the power generators were assumed to be operating under emergency conditions as a worst-case scenario. The general activities included in the operations scenario include:

- Full operation of the ISR plant,
- Full operation of the freeze plant (6 out of 6 units operating),
- Drill rigs operating in the wellfield,
- Operation of a concrete batch plant and crusher,
- Deposit of drill waste in the clean waste pile,
- Power supplied by two (2) 1.1 MW generator sets, operating near the Freeze Plant and ISR plant,
- Power supplied by two (2) 450 kW generator sets, operating near the accommodations centre and the operations centre,
- Electrical utilities operating (i.e., transformers),
- Shipping of yellowcake product,
- Various vehicle movements (fuel, food, raw materials, on-site traffic), and
- Air traffic associated with personnel changes.

The detailed source inventory for the Operations scenario, and approach to the characterization of each source are discussed in Section 3.0.

3.0 SOURCE CHARACTERIZATION

The inventory of noise sources for the Construction and Operations scenarios were developed using information provided by Denison. This information included the process flow diagrams, planned construction fleet, initial equipment lists for the ISR process, freeze plant and utilities, as well as information on the process outlined in the Prefeasibility Study [1] and the Project Description [2] reports. The sound power levels (a measure of the sound energy output of a source) were then derived for each identified source based on available information and/or conservative assumptions.

Sound power levels were generally established using manufacturer specifications, historic measurement data from similar sites, or engineering calculation methods referenced from scientific literature. The inputs for the calculations were derived from available manufacturer specifications and the equipment lists provided by Denison. The list of noise sources associated with the Site Construction and Operation scenarios are summarized in Table 1 and Table 2, respectively. These tables provide an indication of the method used to characterize the sound output of the source, as well as a summary of the key parameters used to estimate the sound levels. As a conservative measure, all power ratings for equipment identified in the Denison equipment list for the ISR process were doubled.

| Activity | Noise Sources | Method (See Notes) | Key Parameters |
|------------------------------|--|--------------------------|---------------------------------------|
| Surface | Crane operation | 1 | 260 hp |
| construction | Concrete batch plant/crusher | 1, 2 | 750 hp |
| | Haul truck loading | 1 | 116 hp wheel loader |
| | Skid steer operation | 1 | 47 hp |
| Freeze plant | Brine circulation pump (x3) | 3 | 100 hp, 1800 rpm |
| (partial | Air-cooled condenser (x2) | 4 | 3 hp per fan, 12 fans per unit |
| operation | Building radiated noise (x2 chillers) | 5,6 | 310-ton cooling capacity each |
| | Haul truck loading | 1 | 116 hp wheel loader |
| Wellfield | Skid steer operation (x2) | 1 | 47 hp (each) |
| activity | Bulldozer operation | 1 | 913 hp |
| | Wheel loader activity | 1 | 116 hp |
| | Mud rotary drill rig | 1 | 470 hp |
| | Diamond drill rig | 1 | 525 hp |
| Clean waste pile activity | Bulldozer operation | 1 | 913 hp |
| | Wheel loader operation | 1 | 116 hp |
| Power | 1.1 MW generators (x2) | 7 | 1.1 MW, 1800 rpm, turbocharged |
| generation | 450 kW generators (x2) | 8 | CAT C15 |
| Fuelling | Propane pumps (x2) | 3 | 25 hp, 1800 rpm |
| Traffic | Fuel/propane deliveries | 9 | 7.5 trucks/day, 35 kph |
| | Food deliveries | 9 | 2 trucks/day, 35 kph |
| | Surface construction deliveries | 9 | 7.5 trucks/day, 35 kph |
| | Wellfield deliveries | 9 | 6 trucks/day, 35 kph |
| | Wellfield mobilizations | 9 | 30 trucks/day, 35 kph |
| | Drill waste to clean waste pile | 9 | 14.5 trips/day (wheel loader), 35 kph |
| | ISR construction – haul truck to clean waste pile | 9 | 24 trucks/day, 35 kph |
| | Freeze plant const. – haul truck to clean waste pile | 9 | 24 trucks/day, 35 kph |
| | Crew van between camp and airstrip | 9 | 5 trips/day, 35 kph |
| | Crew van between camp and Operations Centre | 9 | 20 trips/day, 35 kph |
| | Crew van between camp and ISR site | 9 | 20 trips/day, 35 kph |
| | Air traffic to and from site | 10 | 9 flights per week |

Table 1: Noise Source Inventory for Site Construction

Notes:

1: Diesel engine [3]; 2: IEC database; 3: Pumps [3]; 4: Air-cooled condensers [4]; 5: Chillers [4]; 6: Building radiated noise (interior to exterior) [5]; 7: Diesel generator [3]; 8: Manufacturer data; 9: FHWA on-road vehicles [4]; 10: Integrated Noise Model (INM) [6].

| Activity | Noise Sources | Method | Key Parameters |
|------------------------------|--|-------------|---|
| | | (See Notes) | |
| ISR plant | Building radiated noise: process area | 1, 2, 3 | Interior SPL calculated at 90.2 dBA |
| operations | Building radiated noise: dryer area | 1, 2, 3 | Interior SPL calculated at 97.6 dBA |
| Freeze plant (full | Brine circulation pump (x3) | 1 | 100 hp, 1800 rpm |
| operation) | Air-cooled condenser (x6) | 4 | 3 hp per fan, 12 fans per unit |
| | Building radiated noise (x6 chillers) | 3, 5 | 310-ton cooling capacity each |
| Wellfield activity | Wheel loader activity | 6 | 116 hp |
| | Mud rotary drill rig | 6 | 470 hp |
| | Diamond drill rig | 6 | 525 hp |
| | Building radiated noise: pumphouse | 3 | Interior SPL assumed to be 85 dBA |
| | Wellfield to ISR booster pumps (x4) | 1 | 100 hp |
| Concrete production | Concrete batch plant and crusher | 6, 7 | 750 hp |
| Clean waste pile activity | Wheel loader operation | 6 | 116 hp |
| Fuelling | Propane pumps (x2) | 1 | 25 hp, 1800 rpm |
| Power generation | 1.1 MW generators (x2) | 8 | 1.1 MW, 1800 rpm, turbocharged |
| | 450 kW generators (x2) | 9 | CAT C15 |
| Utilities | Main substation transformer (x1) | 10 | 12.5 MVA |
| | ISR air compressors transformer (x1) | 10 | 3 MVA |
| | ISR plant transformers (x2) | 10 | 1 MVA |
| | Freeze plant modules transformer (x1) | 10 | 7.5 MVA |
| | Freeze plant pumps/controls transformer (x1) | 10 | 1 MVA |
| | Operations Centre transformer (x1) | 10 | 1 MVA |
| | Camp transformer (x1) | 10 | 1 MVA |
| Traffic | Yellowcake shipping | 11 | 2.5 trucks/day, 35 kph |
| | Reagent deliveries | 11 | 10 trucks/day, 35 kph |
| | Fuel/propane deliveries | 11 | 7.5 trucks/day, 35 kph |
| | Food deliveries | 11 | 2 trucks/day, 35 kph |
| | Material deliveries | 11 | 3 trucks/day, 35 kph |
| | Wellfield deliveries | 11 | 3 trucks/day, 35 kph |
| | Wellfield mobilizations | 11 | 30 trucks/day, 35 kph |
| | Drill waste to clean waste pile | 11 | 9.6 trips/day (wheel loader), 35 kph |

Table 2: Noise Source Inventory for Operations

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| Activity | Noise Sources | Method (See Notes) | Key Parameters |
|----------|------------------------------------|-----------------------|----------------------|
| | Crew van between camp and airstrip | 11 | 5 trips/day, 35 kph |
| | Crew van between camp and Ops Ctr. | 11 | 20 trips/day, 35 kph |
| | Crew van between camp and ISR site | 11 | 20 trips/day, 35 kph |
| | Air Traffic to and from site | 12 | 4.5 flights per week |

Notes: 1: Pumps [3]; 2: Electric motors [3]; 3: Building-radiated noise (interior to exterior) [5]; 4: Air-cooled condensers [4]; 5: Chillers [4]; 6: Diesel engines [3]; 7: IEC Database; 8: Diesel Generator [3]; 9: Manufacturer data; 10 Transformers [3]; 11: FHWA on-road vehicles [4]; 12: Integrated Noise Model [6].

A detailed source summary table is provided in Appendix A, which shows all of the sources included in the predictive modelling and an indication of whether they were active for the Construction scenario, the Operations scenario, or both, the overall sound power level, as well as the octave band data.

4.0 PREDICTIVE MODELLING

The propagation of sound from Project activities associated with the Site Construction and Operations scenarios was predicted using the software package Cadna-A, from DataKustik GmbH [5]. The calculation methodology that is implemented in the Cadna-A model is based directly on ISO Standard 9613-2 *Acoustics – Attenuation of sound during propagation outdoors – Part 2: General method of calculation* [7], which is the calculation standard recommended under the Alberta Directive that has been adopted in this assessment [8]. This model can also be used to predict the Ldn metric required under the Health Canada guidance [9]. Air traffic was also assessed within the same Cadna-A model, using a module [6] that implements the Integrated Noise Model (INM) developed by the Federal Aviation Administration (FAA) in the United States.

The premise of the ISO standard, and therefore of the predictive model used in this assessment, is to quantify the various ways in which the sound energy from a noise source (e.g., a drill rig) attenuates as it reaches a receptor (e.g., an off-site cabin). The attenuation parameters include the attenuation due to distance (geometrical divergence), attenuation due to the atmosphere (e.g., relative humidity, temperature), attenuation due to the intervening ground type¹, and attenuation due to obstacles such as natural terrain variations, buildings, or barrier walls. Other parameters that factor into the calculation include source directivity², and the effect of other meteorological conditions such as wind. The model calculates the sound attenuation between all sources and all receptors input to the model, and logarithmically sums the individual source contributions at each receptor to provide an overall predicted sound level for each receptor. In a similar manner, a receptor grid can be established in the model space, with the same calculation occurring at each node point. This data can then be used to visually plot the sound propagation from the facility being modelled as a contour map.

¹ Note this may also be a negative attenuation (i.e., a reflection). For example, if the ground between a source and receptor is hard, such as pavement, or otherwise acoustically reflective, such as water.

² While many sources are omnidirectional (e.g., a pump would be expected to radiate sound equally in all directions), others are directional (e.g., vertical stacks with airflow that directs the noise upwards).

4.1 MODEL CONFIGURATION

The spatial bounds that have been selected for the assessment, as presented in the EIS, are physically represented in the model space. A scaled 3D representation of the facility and its surroundings are constructed in the model using digital terrain mapping and information on the planned building layouts. This is typically scaled using the UTM coordinate system, for ease of exporting and importing data to and from various mapping software (e.g., GIS, AutoCAD, plotting software). The model space is then further populated with the noise sources that have been identified in the inventorying process described in Section 3.0, and the sound power levels established for these sources are assigned. Similarly, the identified sensitive points of reception that are within the LSA are plotted at the coordinates that have been established.

The temporal bounds that have been discussed in the EIS are represented in two ways:

- Establishing the assessment scenarios (i.e., with regard to the project phase being assessed); and
- Configuring the reference time for the predictions in the model.

The assessment scenarios are configured by inputting all of the identified noise sources to the model, and then identifying those associated with the Construction scenario, the Operations scenario, and which are operational in both scenarios. Controls are then set up in the model to automatically switch sources (and any other related infrastructure, if applicable³) on and off, depending on the scenario that is being run.

The temporal boundaries for the predictions are established in the model configuration by establishing the reference times for calculations. Reference times were established in accordance with the guidance documents, which identify that the Ld is the 15-hour period between 07:00 and 22:00, Ln is the 9-hour period between 22:00 and 07:00, and the Ldn is the 24-hour period that combines the Ld and Ln, with a +10 dB penalty for night-time hours [9]. Since the +10 dB penalty is inherent in the Ldn metric (i.e., the Ldn definition includes the +10 dB penalty), the model automatically accounts for it when this parameter is selected for assessment.

There are a number of other configuration parameters that affect the model predictions. These have been set to with the objective of maximizing the conservatism of the calculations, while also reasonably reflecting conditions at the site. These parameters are discussed briefly in Table 3.

³ For example, the Operations scenario will include the ISR plant as a fully constructed building; however, this building would not yet be constructed in the Site Construction scenario. As such, the controls would be set in the model to turn off not only the ISR Operations sources in the Site Construction run, but also the building itself.

| Parameter | Setting | Rationale |
|-------------------------------------|-----------------------|---|
| Temperature, relative humidity | 10°C, 90% | Resulted in maximum predictions |
| Wind | default | ISO 9613-2 calculations assume a moderate downwind condition for all receptor noise calculations (up to 5 m/s [18 km/h]) |
| Orders of reflection ^[1] | 3 | Typical setting for a conservative assessment |
| Surface absorption ^[2] | 0.37 | Buildings set to "Structured Façade", which uses an absorption coefficient of 0.37 (or 2 dB reflection loss). |
| Ground absorption | Global: 1 Local: 0 | The global setting was set to 1 (absorptive) as much of the surrounding area is vegetated. Reflective surfaces such as the Project site and waterbodies were set to 0 (reflective). |
| Receptor heights | 1.5 m above grade | All receptors were assumed to be at an average standing height, which is typically considered to be 1.5 m for such assessments. |

Table 3: Miscellaneous Acoustic Model Configuration Settings

Notes:

[1] "Orders of reflection" refers to how many reflections the model will consider when determining possible source-receptor paths.[2] A measure of the amount of sound energy that is lost (or absorbed) when sound reflects off of a surface such as a building wall.

4.2 SOURCE CONFIGURATION

4.2.1 Industrial Sources

There are four main industrial source types available in the model: point sources, line sources, horizontal area sources, and vertical area sources. Each of the sources identified in the development of the source inventories was assigned the source type that most accurately matched its physical characteristics. Examples of point sources include stack tips, pumps, and stationary equipment such as drill rigs. Line sources were used to define the vehicle traffic routes, and the vehicles were then set up as moving points along those lines and assigned the associated number of trips per hour calculated for each. Horizontal area sources have been used to represent the roofs of buildings (radiating noise from sources operating within), and designated areas within which the pieces of mobile equipment were assumed to be operating. Vertical area sources are generally used to represent building walls that are radiating noise from sources operating within (or sides of enclosures, such as those for the generator units).

The sound power levels associated with the sources that represent the building envelopes were calculated by first establishing the interior sound pressure level expected in the building, and then estimating the transmission of sound through the applicable building component (wall or roof). The interior sound pressure level is established using the sound power levels of the sources operating inside of the building, as well as the reflective characteristics of the interior building surfaces. The building is then enveloped with area sources, and the interior sound level is used with the transmission loss of the building component to calculate the sound power level of the exterior surface. The transmission losses were based on 16-gauge steel panel, with the exception of the generator enclosures, which were based on fibreglass reinforced panels (FRP) per the design information provided by Denison. Images of the model set-up, rendered in 3D, are provided in Figure 1 and Figure 2.

4.2.2 Air Traffic Sources

Noise caused by flights arriving and departing the airstrip were assessed using the FLG module in Cadna-A [6], which implements the algorithms from the FAA air traffic noise model INM. INM includes a database of commercial aircraft that are in common use in North America, inclusive of sound power and directivity during both departure and approach. The airstrip was positioned in the model using a reference coordinate, its magnetic headings and proposed length of 1,600 m. It was assumed that flights may arrive and depart either from the north or south, resulting the development of four distinct air routes. The fleets for the various carriers that service northern Saskatchewan mines were reviewed, and a representative aircraft was selected for crew changes. The ATR-42 is a turbo-prop aircraft in common use for regional transport to mine sites and carries up to 52 personnel so is typical for crew changes. The de Havilland DASH 8 is an equivalent aircraft which appears in the INM database and was applied in this assessment. Denison anticipates up to nine flights per week, while the model is configured to predict the maximum 24-hour period. To be conservative, it was assumed that there could be four flights arriving and departing in the same 24-hr period. These were split evenly between among the defined air routes.



Figure 1: 3D Model View (Looking West)



Figure 2: 3D Model View (Looking South-West)

4.3 POINTS OF RECEPTION

Points of reception are discrete locations at which sound levels are predicted in the modelling. These represent the locations at which the sound environment has been identified as a VC, and therefore at which the assessment of noise effects will be evaluated. There are no communities located near to the Project site. The nearest community in terms of straight-line distance is the northern settlement of Wollaston Lake and the neighbouring reserve of Lac La Hache, which are approximately 150 km away. The nearest community in terms of access by road is Pinehouse, which is approximately 260 km away.

There are a number of lease areas in the vicinity of the Project site, and it has been assumed that these contain cabins for purposes of this assessment. As such, these locations have been included as points of reception in the model if they are located within the LSA. In addition, locations of interest to the *Human Health and Ecological Risk Assessment* have been included in the model, which include various types of human locations (nearest seasonal residence, trapping location, and worker camp), and an ecological location. It should be noted that the ecological risk location (Risk1) has not been assessed in against the adopted criteria, which is for human receptors only. In addition, the camp location (Risk3) has not been assessed against the adopted criteria, as it is on-site and associated with the Project, and therefore not representative of a sensitive community. A map depicting the locations of sensitive receptors used in this assessment is included in Figure 3.



5.0 MODELLING RESULTS

5.1 FEDERAL GUIDANCE

The Health Canada criteria for noise assessment include both an absolute limit of 75 dBA (Ldn), and a relative limit of an increase in %HA of no greater than 6.5% [9]. The conservative assessment scenarios defined in Section 3.0 were modelled in accordance with the procedures detailed in Section 4.0, and the results of this assessment are summarized in Table 4.

The predicted future Ldn values at the leased properties were generally predicted to remain equal to or within 0.4 dBA of the baseline levels during both construction and operations, with the exception of one leased location (302586) and one risk location (Risk2), which are located on the same property. Property 302586 is a seasonal cabin located to the south-east of the Wheeler River site, at the edge of McGowan Lake. This location is approximately 1.3 km from the access road connecting to Highway 914. The baseline Ldn of 37.6 dBA applied at the sensitive receptors in this assessment does not include haulage of ore between McArthur River and Key Lake on Highway 914, as this activity has not occurred since 2017 (see Section 6.2.3 of the EIS). If such traffic were to resume, there is potential for the baseline level to increase at this location, which would also increase the baseline %HA and thereby increase the potential for an exceedance of the Health Canada criteria. Based on traffic volumes documented as part of the Millennium Project EA and summarized in a memo prepared by Denison [10], the estimated daily truck traffic on Highway 914 when McArthur River and Key Lake are operating is approximately 58 trucks per day. A model was prepared that estimated the contributing sound levels of this amount of traffic on Highway 914 at each of the sensitive receptors included in the assessment. At location 302586/Risk2 the predicted Ldn due to truck traffic was 18.3 dBA, which would not change the predicted sound levels when added on a logarithmic basis and therefore not change the assessment results based on the Health Canada Guideline.

At Property 302586, the baseline Ldn was predicted to increase by 4.7 dBA during construction, from 37.6 dBA to 42.3 dBA. In terms of %HA, this represents a +0.4% difference. If the baseline and future Ldn values are increased by +10 dB each, per Health Canada recommendation for locations that are expected to be highly sensitive to noise, the increase in %HA at this location changes to +1.3%. The increase is primarily related to the use of heavy equipment in the development of the wellfield and the generators, as well as truck traffic accessing the site from Highway 914. During operations, the increase from baseline at this location was predicted to be 2.8 dBA, from 37.6 dBA to 40.4 dBA. When these are adjusted by +10 dB as above, the resulting change in %HA is +0.7%. During operations, the sound levels at this location are attributable to the heavy equipment operating in the wellfield, use of the emergency generators (included as a worst-case scenario), and traffic along the access road from Highway 914.

The predictive modelling indicates that the Project does not cause an adverse effect with regard to the Health Canada Guideline at any of the identified receptors, as the future conditions remain below 75 dBA and the %HA does not increase by more than 6.5% at any receptor identified.

Contour plots depicting the sound propagation (in Ldn) and increase in %HA from the Construction and Operations phases are provided in Figure 4 to Figure 7. Note that these represent the predicted noise from the site added to the baseline Ldn of 37.6 dBA. These plots show that the sound level contours during construction

and operations return to the baseline level within the LSA, with the exception of a small extension to the northeast which is associated with the daytime incoming/outgoing flights at the airstrip. During construction, the Ldn sound levels are predicted to return to background within approximately 6 kilometres of main activity areas, while the Operations Ldn sound levels are predicted to return to background within approximately 4 kilometres of the main activity areas.

5.2 **PROVINCIAL GUIDANCE**

The PSLs for the Project under the Alberta Directive are 40 dBA (Ld) and 36 dBA (Ln). The conservative assessment scenarios defined in Section 2.0 were modelled in accordance with the procedures detailed in Section 4.0 to predict Ld and Ln sound levels at each identified receptor, and the results of this assessment are summarized in Table 5 and Table 6.

At the leased properties, the sound levels generally remained equal to the baseline sound level, or increased by less than 0.5 dBA, with the exception of the property identified as 302586/Risk2. As noted in the previous section, this receptor is located to the south-east of the Wheeler River site, adjacent to McGowan Lake. During construction, the daytime and night-time sound levels increased over baseline conditions by 5.1 dBA and 4.6 dBA, respectively, and the future levels were found to be less than the established PSLs. The increases in sound level at this location are primarily associated with the construction equipment being used in the development of the wellfield. During operations, the increases are 3.4 dBA and 2.8 dBA during the daytime and night-time, respectively, and are predicted to be below the PSLs.

Contour plots depicting the sound propagation in Ld and Ln for both Construction and Operations are provided in Figure 8 to Figure 11. Note that these depict the future predicted sound levels from the site activities added to the ambient sound levels discussed in Section 6.2.3 of the EIS. The extent of displayed contours represents the return to the established baseline conditions, while the applicable PSL is shown as a blue line. During both construction and operations, the daytime and night-time sound levels are predicted to return to baseline conditions within the LSA, with the exception of some influence of the flight paths associated with use of the airstrip during the daytime hours. The PSLs for daytime and night-time during construction are met within 2 km and 2.5 km of the main activity area at the site, respectively; both of which are well within the LSA spatial boundary. During operations, the PSLs are met within approximately 1 km during the daytime, and 1.5 km during the night-time.

| Name | ID | Basel | ine Condit | ion ⁽¹⁾ | | С | onstructio | n | | | | Operation | 5 | |
|--|--------|-------|-----------------------------|--------------------|-------|-----------------------------|-----------------------------|-----|------|-------|-----------------------------|-----------------------------|-----|------|
| | | Ldn | Ldn- Adj. ⁽²⁾ | %HA | Ldn | Total Ldn ⁽³⁾ | Ldn- Adj. ⁽²⁾ | %HA | Δ%НА | Ldn | Total Ldn ⁽³⁾ | Ldn- Adj. ⁽²⁾ | %HA | Δ%НА |
| | | (dBA) | (dBA) | | (dBA) | (dBA) | (dBA) | | | (dBA) | (dBA) | (dBA) | | |
| Leased property | 300601 | 37.6 | 47.6 | 1.6 | 21.3 | 37.7 | 47.7 | 1.6 | 0.0 | 18.9 | 37.7 | 47.7 | 1.6 | 0.0 |
| Leased property | 301493 | 37.6 | 47.6 | 1.6 | 26.4 | 37.9 | 47.9 | 1.7 | 0.1 | 23.0 | 37.7 | 47.7 | 1.6 | 0.0 |
| Leased property | 302424 | 37.6 | 47.6 | 1.6 | 14.4 | 37.6 | 47.6 | 1.6 | 0.0 | 14.5 | 37.6 | 47.6 | 1.6 | 0.0 |
| Leased property | 302586 | 37.6 | 47.6 | 1.6 | 40.4 | 42.3 | 52.3 | 2.9 | 1.3 | 37.3 | 40.4 | 50.4 | 2.3 | 0.7 |
| Leased property | 302955 | 37.6 | 47.6 | 1.6 | 10.9 | 37.6 | 47.6 | 1.6 | 0.0 | 10.9 | 37.6 | 47.6 | 1.6 | 0.0 |
| Leased property | 303010 | 37.6 | 47.6 | 1.6 | 6.2 | 37.6 | 47.6 | 1.6 | 0.0 | 6.2 | 37.6 | 47.6 | 1.6 | 0.0 |
| Leased property | 303069 | 37.6 | 47.6 | 1.6 | 14.0 | 37.6 | 47.6 | 1.6 | 0.0 | 14.0 | 37.6 | 47.6 | 1.6 | 0.0 |
| Leased property | 303109 | 37.6 | 47.6 | 1.6 | 6.4 | 37.6 | 47.6 | 1.6 | 0.0 | 6.4 | 37.6 | 47.6 | 1.6 | 0.0 |
| Leased property | 303238 | 37.6 | 47.6 | 1.6 | 11.8 | 37.6 | 47.6 | 1.6 | 0.0 | 11.8 | 37.6 | 47.6 | 1.6 | 0.0 |
| Leased property | 602377 | 37.6 | 47.6 | 1.6 | 16.6 | 37.6 | 47.6 | 1.6 | 0.0 | 16.6 | 37.6 | 47.6 | 1.6 | 0.0 |
| Risk - ecological on-site ⁽⁴⁾ | Risk1 | 37.6 | N/A | N/A | 59.4 | 59.4 | N/A | N/A | N/A | 45.7 | 46.3 | N/A | N/A | N/A |
| Risk - human: trapper | Risk2 | 37.6 | 47.6 | 1.6 | 40.4 | 42.3 | 52.3 | 2.9 | 1.3 | 37.3 | 40.4 | 50.4 | 2.3 | 0.7 |
| Risk - human: camp worker ⁽⁴⁾ | Risk3 | 37.6 | N/A | N/A | 51.6 | 51.8 | N/A | N/A | N/A | 51.7 | 51.9 | N/A | N/A | N/A |
| Risk - human: seasonal resident | Risk4 | 37.6 | 47.6 | 1.6 | 27.0 | 38.0 | 48.0 | 1.7 | 0.1 | 24.4 | 37.8 | 47.8 | 1.6 | 0.0 |
| Risk - reference receptor location | Risk5 | 37.6 | 47.6 | 1.6 | 34.6 | 39.4 | 49.4 | 2.0 | 0.4 | 32.0 | 38.7 | 48.7 | 1.8 | 0.2 |

| Table 4: Health Canada Guideline Effects Assessment | (Construction and Operations) |
|--|-------------------------------|
|--|-------------------------------|

Notes:

(1) The baseline condition (or background condition) was established in the measurement program discussed in Section Error! Reference source not found. and summarized in Error! Reference source not found.

(2) Per Health Canada guidance, the measured/predicted Ldn should be adjusted by +10 dBA for quiet rural or remote settings [9]

(3) The "Total Ldn" represents the baseline Ldn added logarithmically to the model-predicted Ldn

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| Name | ID | Basel | Baseline Condition ⁽¹⁾ | | | C | onstructio | n | | | | Operations | ; | |
|--------------------------------------|--|-------|-------------------------------------|--|-------|-----------------------------|-----------------------------|-----|------|-------|-----------------------------|-----------------------------|-----|------|
| | | Ldn | Ldn Ldn- Adj. ⁽²⁾ %HA | | | Total Ldn ⁽³⁾ | Ldn- Adj. ⁽²⁾ | %HA | Δ%НА | Ldn | Total Ldn ⁽³⁾ | Ldn- Adj. ⁽²⁾ | %HA | Δ%НА |
| | | (dBA) | (dBA) | | (dBA) | (dBA) | (dBA) | | | (dBA) | (dBA) | (dBA) | | |
| (4) These are not receptors in terms | 4) These are not receptors in terms of the Health Canada Guideline, and so only the model results are displayed. | | | | | | | | | | | | | |

Table 5: Alberta Directive Effects Assessment (Construction)

| Name | ID | Baseline Condition | | Construc | tion Only | Total Cor | nstruction 3) | P | SL | Diffe (Total | rence – PSL) |
|--|--------|--------------------|-------|----------|-----------|-----------|------------------|-------|-------|-----------------|-----------------|
| | | Day | Night | Day | Night | Day | Night | Day | Night | Day | Night |
| | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) |
| Leased property | 300601 | 30.7 | 31.3 | 17.6 | 14.2 | 30.9 | 31.4 | 40 | 36 | -9.1 | -4.6 |
| Leased property | 301493 | 30.7 | 31.3 | 21.7 | 19.7 | 31.2 | 31.6 | 40 | 36 | -8.8 | -4.4 |
| Leased property | 302424 | 30.7 | 31.3 | 16.3 | 0 | 30.9 | 31.3 | 40 | 36 | -9.1 | -4.7 |
| Leased property | 302586 | 30.7 | 31.3 | 34.2 | 34.0 | 35.8 | 35.9 | 40 | 36 | -4.2 | -0.1 |
| Leased property | 302955 | 30.7 | 31.3 | 12.8 | 0 | 30.8 | 31.3 | 40 | 36 | -9.2 | -4.7 |
| Leased property | 303010 | 30.7 | 31.3 | 8.3 | 0 | 30.7 | 31.3 | 40 | 36 | -9.3 | -4.7 |
| Leased property | 303069 | 30.7 | 31.3 | 15.9 | 0 | 30.8 | 31.3 | 40 | 36 | -9.2 | -4.7 |
| Leased property | 303109 | 30.7 | 31.3 | 8.5 | 0 | 30.7 | 31.3 | 40 | 36 | -9.3 | -4.7 |
| Leased property | 303238 | 30.7 | 31.3 | 13.7 | 0 | 30.8 | 31.3 | 40 | 36 | -9.2 | -4.7 |
| Leased property | 602377 | 30.7 | 31.3 | 18.7 | 0 | 31.0 | 31.3 | 40 | 36 | -9.0 | -4.7 |
| Risk - ecological on-site ⁽⁴⁾ | Risk1 | 30.7 | 31.3 | 53.0 | 53.0 | 53.1 | 53.0 | N/A | N/A | N/A | N/A |
| Risk - human: trapper | Risk2 | 30.7 | 31.3 | 34.2 | 34.0 | 35.8 | 35.9 | 40 | 36 | -4.2 | -0.1 |
| Risk - human: camp worker ⁽⁴⁾ | Risk3 | 30.7 | 31.3 | 45.3 | 45.2 | 45.4 | 45.4 | N/A | N/A | N/A | N/A |

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| Name | ID | Baseline Condition | | Construc | tion Only | Total Con | struction | PS | SL | Differ (Total | rence – PSL) |
|------------------------------------|-------|--------------------|------|----------|-----------|-----------|-----------|-------|-------|------------------|-----------------|
| | | Day Night | | Day | Night | Day | Night | Day | Night | Day | Night |
| | | (dBA) (dBA) | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) |
| Risk - human: seasonal resident | Risk4 | 30.7 | 31.3 | 21.6 | 20.4 | 31.2 | 31.6 | 40 | 36 | -8.8 | -4.4 |
| Risk - reference receptor location | Risk5 | 30.7 | 31.3 | 28.3 | 28.2 | 32.7 | 33.0 | 40 | 36 | -7.3 | -3.0 |

Notes:

(1) The Baseline Condition (or background condition) was established in the measurement program discussed in Section Error! Reference source not found. and summarized in Error! Reference source not found.

(2) The Construction Only sound level is the contribution from the Project only, determined via predictive modelling.

(3) The Total Construction sound level is the logarithmic addition of the baseline sound level to the modelled project sound level.

(4) These receptors are not community locations and therefore only the modelling results are displayed.

Table 6: Alberta Directive Effects Assessment (Operations)

| Name | ID | Baseline (| Condition | Operatio | ns Only ⁽²⁾ | Total Ope | erations ⁽³⁾ | P | SL | Differ (Total | ence – PSL) |
|-----------------|--------|------------|-----------|----------|------------------------|-----------|-------------------------|-------|-------|------------------|----------------|
| | | Day | Night | Day | Night | Day | Night | Day | Night | Day | Night |
| | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) |
| leased property | 300601 | 30.7 | 31.3 | 16.6 | 11.1 | 30.9 | 31.3 | 40 | 36 | -9.1 | -4.7 |
| leased property | 301493 | 30.7 | 31.3 | 19.8 | 15.7 | 31.0 | 31.4 | 40 | 36 | -9.0 | -4.6 |
| leased property | 302424 | 30.7 | 31.3 | 16.3 | 0 | 30.9 | 31.3 | 40 | 36 | -9.1 | -4.7 |
| leased property | 302586 | 30.7 | 31.3 | 31.4 | 30.7 | 34.1 | 34.0 | 40 | 36 | -5.9 | -2.0 |
| leased property | 302955 | 30.7 | 31.3 | 12.8 | 0 | 30.8 | 31.3 | 40 | 36 | -9.2 | -4.7 |
| leased property | 303010 | 30.7 | 31.3 | 8.3 | 0 | 30.7 | 31.3 | 40 | 36 | -9.3 | -4.7 |
| leased property | 303069 | 30.7 | 31.3 | 15.9 | 0 | 30.8 | 31.3 | 40 | 36 | -9.2 | -4.7 |
| leased property | 303109 | 30.7 | 31.3 | 8.5 | 0 | 30.7 | 31.3 | 40 | 36 | -9.3 | -4.7 |
| leased property | 303238 | 30.7 | 31.3 | 13.7 | 0 | 30.8 | 31.3 | 40 | 36 | -9.2 | -4.7 |

| Name | ID | Baseline Condition | | Operatio | ns Only ⁽²⁾ | Total Ope | erations ⁽³⁾ | P | SL | Differ (Total | rence – PSL) |
|--|--------|--------------------|-------|----------|------------------------|-------------|-------------------------|-------|-------|------------------|-----------------|
| | | Day | Night | Day | Night | Day | Night | Day | Night | Day | Night |
| | | (dBA) | (dBA) | (dBA) | (dBA) | (dBA) (dBA) | | (dBA) | (dBA) | (dBA) | (dBA) |
| leased property | 602377 | 30.7 | 31.3 | 18.7 | 0 | 31.0 | 31.3 | 40 | 36 | -9.0 | -4.7 |
| risk - ecological on-site ⁽⁴⁾ | Risk1 | 30.7 | 31.3 | 41.5 | 38.7 | 41.8 | 39.4 | N/A | N/A | N/A | N/A |
| risk - human: trapper | Risk2 | 30.7 | 31.3 | 31.4 | 30.8 | 34.1 | 34.1 | 40 | 36 | -5.9 | -1.9 |
| risk - human: camp worker ⁽⁴⁾ | Risk3 | 30.7 | 31.3 | 45.3 | 45.2 | 45.4 | 45.4 | N/A | N/A | N/A | N/A |
| risk - human: seasonal resident | Risk4 | 30.7 | 31.3 | 19.9 | 17.6 | 31.0 | 31.5 | 40 | 36 | -9.0 | -4.5 |
| risk - reference receptor location | Risk5 | 30.7 | 31.3 | 26.0 | 25.5 | 32.0 | 32.3 | 40 | 36 | -8.0 | -3.7 |

















6.0 RECOMMENDED CONSTRUCTION PRACTICES

The following construction practices are recommended based on industry best practices for reducing the likelihood of impacts during construction projects.

Administrative controls

- Planning truck routes to minimize separation distance to the nearest receptors,
- Maximizing the distance between the planned construction staging areas and equipment locations and the sensitive receptors,
- Planning to use the least impactful construction method available,
- Ensuring those potentially impacted by construction noise are aware of how to lodge complaints,
- Complete regular inspections of equipment to ensure it is in good working order, and
- Minimize night-time operations.

Physical controls

- Select mobile construction equipment that is appropriately sized for its task,
- Ensure all exhausts (e.g., mobile equipment, generators) are outfitted with effective muffling devices that are in good working condition,
- Selecting low-noise tools and equipment where available,
- Avoid dropping material from height, and
- Turn off equipment when not being used.

7.0 REFERENCES

- [1] Denison Mines, "Prefeasibility Study Report for the Wheeler River Uranium Project Saskatchewan Canada," Denison Mines, Saskatoon, 2018.
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- [4] L. Miller, "Noise Control for Buildings and Manufacturing Plants," Bolt Beranek and Newman Inc., Cambridge, 1981.
- [5] DataKustik GmbH, "Cadna-A Reference Manual (Version 2021 MR1)," DataKustik, Gilching, 2020.
- [6] DataKustik GmbH, "Introduction to Cadna-A INM," DataKustik, 2013.
- [7] International Organization for Standardization (ISO), "Acoustics Attenuation of sound during propagation outdoors Part 2: General method of calculation," ISO, Geneva, 1996.
- [8] Alberta Energy Regulator (AER), "Directive 038: Noise Control," AER, Calgary, 2007 (Updated 2013).
- [9] Health Canada, "Guidance for Evaluating Human Health Impacts in Environmental Assessment: Noise," Health Canada, Ottawa, 2017.
- [10] Denison Mines, "Memorandum re: Traffic Volumes," February 10, 2021.

Appendix A:

Assessment Scenarios and Sound Level Data



Table A-1: Assessment Scenarios and Sound Level Data

| Source ID | Source Description | Number of | Sound | Active S | itatus | | | Octave Ban | d Centre Fre | quency (Hz); | Sound Powe | er Level (dB) | | | Ονε | erall |
|---------------------|--|-----------|-------------|--------------|------------|------|-------|------------|--------------|--------------|------------|---------------|-------|------|-------|-------|
| | | Identical | Power Level | Construction | Operations | 31.5 | 63 | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 | dB | dBA |
| | | Sources | (dBA) | | | | | | | | | | | | | |
| Point Sources | | | | | | | | | | | | | | | | |
| FP_ACC1Fan(x) | Freeze Plant: ACC Unit 1 Fan | 12 | 94.0 | • | • | 94.8 | 97.8 | 97.8 | 94.8 | 91.8 | 87.8 | 84.8 | 81.8 | 73.8 | 103.2 | 94.0 |
| FP_ACC2Fan(x) | Freeze Plant: ACC Unit 2 Fan | 12 | 94.0 | • | • | 94.8 | 97.8 | 97.8 | 94.8 | 91.8 | 87.8 | 84.8 | 81.8 | 73.8 | 103.2 | 94.0 |
| FP_ACC3Fan(x) | Freeze Plant: ACC Unit 3 Fan | 12 | 94.0 | 0 | • | 94.8 | 97.8 | 97.8 | 94.8 | 91.8 | 87.8 | 84.8 | 81.8 | 73.8 | 103.2 | 94.0 |
| FP_ACC4Fan(x) | Freeze Plant: ACC Unit 4 Fan | 12 | 94.0 | 0 | • | 94.8 | 97.8 | 97.8 | 94.8 | 91.8 | 87.8 | 84.8 | 81.8 | 73.8 | 103.2 | 94.0 |
| FP_ACC5Fan(x) | Freeze Plant: ACC Unit 5 Fan | 12 | 94.0 | 0 | • | 94.8 | 97.8 | 97.8 | 94.8 | 91.8 | 87.8 | 84.8 | 81.8 | 73.8 | 103.2 | 94.0 |
| FP_ACC6Fan(x) | Freeze Plant: ACC Unit 6 Fan | 12 | 94.0 | 0 | • | 94.8 | 97.8 | 97.8 | 94.8 | 91.8 | 87.8 | 84.8 | 81.8 | 73.8 | 103.2 | 94.0 |
| Gen1_Exh | Generator 1: Exhaust | 1 | 109.4 | • | • | | 118.1 | 117.1 | 109.1 | 105.1 | 105.1 | 100.1 | 90.1 | 81.1 | 121.2 | 109.4 |
| Gen2_Exh | Generator 2: Exhaust | 1 | 109.4 | • | • | | 118.1 | 117.1 | 109.1 | 105.1 | 105.1 | 100.1 | 90.1 | 81.1 | 121.2 | 109.4 |
| FP_BCP(x) | Freeze Plant: Brine Circulation Pump | 3 | 99.3 | • | • | | 89.7 | 90.7 | 92.7 | 92.7 | 95.7 | 92.7 | 88.7 | 82.7 | 100.9 | 99.3 |
| Const_U_PFP1 | Utilities (Construction): Propane Fuel Pump (ISR Plant) | 1 | 94.6 | • | 0 | | 85.0 | 86.0 | 88.0 | 88.0 | 91.0 | 88.0 | 84.0 | 78.0 | 96.2 | 94.6 |
| Const_U_PFP2 | Utilities (Construction): Propane Fuel Pump (Camp) | 1 | 94.6 | • | 0 | | 85.0 | 86.0 | 88.0 | 88.0 | 91.0 | 88.0 | 84.0 | 78.0 | 96.2 | 94.6 |
| U_PFP1 | Utilities (Operations): Propane Fuel Pump (ISR Plant) | 1 | 94.6 | 0 | • | | 85.0 | 86.0 | 88.0 | 88.0 | 91.0 | 88.0 | 84.0 | 78.0 | 96.2 | 94.6 |
| U_PFP2 | Utilities (Operations): Propane Fuel Pump (Camp) | 1 | 94.6 | 0 | • | | 85.0 | 86.0 | 88.0 | 88.0 | 91.0 | 88.0 | 84.0 | 78.0 | 96.2 | 94.6 |
| U_TMS | Utilities: Main Substation Transformer | 1 | 92.1 | 0 | • | 88.7 | 94.7 | 96.7 | 91.7 | 91.7 | 85.7 | 80.7 | 75.7 | 68.7 | 100.7 | 92.1 |
| U_TFPM | Utilities: Freeze Plant Modules Transformer | 1 | 87.9 | 0 | • | 84.5 | 90.5 | 92.5 | 87.5 | 87.5 | 81.5 | 76.5 | 71.5 | 64.5 | 96.5 | 87.9 |
| U_TFPPC | Utilities: Freeze Plant Pumps/Controls Transformer | 1 | 81.0 | 0 | • | 77.6 | 83.6 | 85.6 | 80.6 | 80.6 | 74.6 | 69.6 | 64.6 | 57.6 | 89.6 | 81.0 |
| U_TISRAC | Utilities: ISR Plant Air Compressors Transformer | 1 | 84.6 | 0 | • | 81.2 | 87.2 | 89.2 | 84.2 | 84.2 | 78.2 | 73.2 | 68.2 | 61.2 | 93.2 | 84.6 |
| U_TISRP(x) | Utilities: ISR Plant Process Transformer | 2 | 81.0 | 0 | • | 77.6 | 83.6 | 85.6 | 80.6 | 80.6 | 74.6 | 69.6 | 64.6 | 57.6 | 89.6 | 81.0 |
| U_TOP | Utilities: Operations Centre Transformer | 1 | 81.0 | 0 | • | 77.6 | 83.6 | 85.6 | 80.6 | 80.6 | 74.6 | 69.6 | 64.6 | 57.6 | 89.6 | 81.0 |
| U_TC | Utilities: Camp Transformer | 1 | 81.0 | 0 | • | 77.6 | 83.6 | 85.6 | 80.6 | 80.6 | 74.6 | 69.6 | 64.6 | 57.6 | 89.6 | 81.0 |
| Const_CranelSR | Construction: Crane at ISR Plant | 1 | 109.2 | • | 0 | | 102.9 | 107.9 | 110.9 | 105.9 | 103.9 | 100.9 | 94.9 | 88.9 | 114.5 | 109.2 |
| Const_CementMix | Construction: Cement Truck/Mixer | 1 | 117.8 | • | 0 | | 111.5 | 116.5 | 119.5 | 114.5 | 112.5 | 109.5 | 103.5 | 97.5 | 123.1 | 117.8 |
| Const_HTLoad_ISR | Construction: Haul Truck Loading (ISR) | 1 | 109.7 | • | 0 | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| Const_HTLoad_FP | Construction: Haul Truck Loading (Freeze Plant) | 1 | 109.7 | • | 0 | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| Const_LoaderCWP2 | Wellfield (Construction): Loader at Clean Waste Pile (Shaping) | 1 | 109.7 | • | 0 | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| Const_WF_LoaderWell | Wellfield (Construction): Loader at Wellfield | 1 | 109.7 | • | 0 | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| Const_WF_LoaderCWP | Wellfield (Construction): Loader at Clean Waste Pile | 1 | 109.7 | • | 0 | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |

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INDEPENDENT ENVIRONMENTAL CONSULTANTS 582 ST CLAIR AVENUE WEST, SUITE 221, TORONTO, ON, MGC 1A6 | TEL: (844) 736-7369

| Source ID | Source Description | Number of | Sound | Active | Status | | | Octave Ban | d Centre Free | quency (Hz); | Sound Powe | r Level (dB) | | | Ove | erall |
|-----------------------------|---|-----------|-------------|--------------|------------|------|-------|------------|---------------|--------------|------------|--------------|-------|------|-------|-------|
| | | Identical | Power Level | Construction | Operations | 31.5 | 63 | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 | dB | dBA |
| | | Sources | (dBA) | | | | | | | | | | | | | |
| WF_LoaderCWP | Wellfield (Operations): Loader at Clean Waste Pile | 1 | 109.7 | 0 | • | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| WF_LoaderWell | Wellfield (Operations): Loader at Wellfield | 1 | 109.7 | 0 | • | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| WF_BP(x) | Wellfield: Booster Pump | 4 | 99.3 | 0 | • | | 89.7 | 90.7 | 92.7 | 92.7 | 95.7 | 92.7 | 88.7 | 82.7 | 100.9 | 99.3 |
| Const_WF_DiamondDrill1 | Wellfield (Construction): Diamond Drill Rig | 2 | 113.2 | • | 0 | | 106.9 | 111.9 | 114.9 | 109.9 | 107.9 | 104.9 | 98.9 | 92.9 | 118.5 | 113.2 |
| Const_WF_MudRotaryDrill1 | Wellfield (Construction): Mud Rotary Drill Rig | 2 | 112.8 | • | 0 | | 106.5 | 111.5 | 114.5 | 109.5 | 107.5 | 104.5 | 98.5 | 92.5 | 118.1 | 112.8 |
| WF_DiamondDrill1 | Wellfield: Diamond Drill Rig (Operations) | 2 | 113.2 | 0 | • | | 106.9 | 111.9 | 114.9 | 109.9 | 107.9 | 104.9 | 98.9 | 92.9 | 118.5 | 113.2 |
| WF_MudRotaryDrill1 | Wellfield: Mud Rotary Drill Rig (Operations) | 2 | 112.8 | 0 | • | | 106.5 | 111.5 | 114.5 | 109.5 | 107.5 | 104.5 | 98.5 | 92.5 | 118.1 | 112.8 |
| Const_Crusher | Wellfield (Construction): Crusher at Borrow Pit | 1 | 120.3 | • | 0 | | 124 | 122 | 122 | 116 | 116 | 115 | 114 | 110 | 128.5 | 120.3 |
| WF_Crusher | Wellfield (Operations): Crusher at Borrow Pit | 1 | 120.3 | 0 | • | | 124 | 122 | 122 | 116 | 116 | 115 | 114 | 110 | 128.5 | 120.3 |
| Line Sources ^[1] | | | • • | | · | | • | | | | | | | | | |
| CTraffic_Fuel | Construction Traffic: Fuel/propane deliveries | 1 | 96.7 | • | 0 | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| CTraffic_Food | Construction Traffic: Food deliveries | 1 | 86.5 | • | 0 | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| CTraffic_Offsite | Construction Traffic: Off-site trucks from Highway 914 to Gate | 1 | 109.6 | • | 0 | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| CTraffic_SurfaceConst | Construction Traffic: Surface construction deliveries | 1 | 96.2 | • | 0 | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| CTraffic_Wellfield | Construction Traffic: Wellfield deliveries | 1 | 93.6 | • | 0 | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| CTraffic_WellMob | Construction Traffic: Wellfield mobilizations | 1 | 100.6 | • | 0 | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| CTraffic_Airstrip | Construction Traffic: Airstrip Traffic | 1 | 87.6 | • | 0 | 95.0 | 98.0 | 102.0 | 101.0 | 98.0 | 94.0 | 91.0 | 84.0 | 77.0 | 106.8 | 99.9 |
| CTraffic_CleanWaste | Construction Traffic: Drill waste to clean pile | 1 | 94.2 | • | 0 | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| CTraffic_VantoOps | Construction Traffic: Crew Van to Operations Centre | 1 | 83.2 | • | 0 | 95.0 | 98.0 | 102.0 | 101.0 | 98.0 | 94.0 | 91.0 | 84.0 | 77.0 | 106.8 | 99.9 |
| CTraffic_VantoISR | Construction Traffic: Crew Van to ISR | 1 | 88.1 | • | 0 | 95.0 | 98.0 | 102.0 | 101.0 | 98.0 | 94.0 | 91.0 | 84.0 | 77.0 | 106.8 | 99.9 |
| CTraffic_HT_ISRCWP | Construction Traffic: Haul Truck, ISR to Clean Waste Pile | 1 | 104.5 | • | 0 | | 110.6 | 115.6 | 118.6 | 113.6 | 111.6 | 108.6 | 102.6 | 96.6 | 122.2 | 116.9 |
| CTraffic_HT_FPCWP | Construction Traffic: Haul Truck, Freeze Plant Clean Waste Pile | 1 | 102.4 | • | 0 | | 110.6 | 115.6 | 118.6 | 113.6 | 111.6 | 108.6 | 102.6 | 96.6 | 122.2 | 116.9 |
| OpsTraffic_Yellowcake | Operations Traffic: Yellowcake shipping | 1 | 91.7 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_Fuel | Operations Traffic: Fuel/propane deliveries | 1 | 96.7 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_Food | Operations Traffic: Food deliveries | 1 | 86.5 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_Materials | Operations Traffic: Materials | 1 | 93.5 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_Offsite | Operations Traffic: Off-site trucks from Highway 914 to Gate | 1 | 110.0 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_Reagents | Operations Traffic: Reagents | 1 | 97.7 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_Wellfield | Operations Traffic: Wellfield deliveries | 1 | 91.4 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |

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| Source ID | Source Description | Number of | Sound | Active S | tatus | | | Octave Ban | d Centre Fred | uency (Hz); | Sound Powe | er Level (dB) | | | Ove | erall |
|-----------------------|--|-----------|-------------|--------------|------------|-------|-------|------------|---------------|-------------|------------|---------------|-------|-------|-------|-------|
| | | Identical | Power Level | Construction | Operations | 31.5 | 63 | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 | dB | dBA |
| | | Sources | (dBA) | | | | | | | | | | | | | |
| OpsTraffic_WellMob | Operations Traffic: Wellfield mobilizations | 1 | 100.6 | 0 | • | | 105.2 | 110.2 | 113.2 | 108.2 | 106.2 | 103.2 | 97.2 | 91.2 | 116.8 | 111.5 |
| OpsTraffic_CleanWaste | Operations Traffic: Drill waste to clean pile | 1 | 92.4 | 0 | • | | 103.4 | 108.4 | 111.4 | 106.4 | 104.4 | 101.4 | 95.4 | 89.4 | 115.0 | 109.7 |
| OpsTraffic_Airstrip | Operations Traffic: Airstrip Traffic | 1 | 87.6 | 0 | • | 95.0 | 98.0 | 102.0 | 101.0 | 98.0 | 94.0 | 91.0 | 84.0 | 77.0 | 106.8 | 99.9 |
| OpsTraffic_VantoISR | Operations Traffic: Crew Van to ISR | 1 | 88.1 | 0 | • | 95.0 | 98.0 | 102.0 | 101.0 | 98.0 | 94.0 | 91.0 | 84.0 | 77.0 | 106.8 | 99.9 |
| OpsTraffic_VantoOps | Operations Traffic: Crew Van to Operations Centre | 1 | 83.2 | 0 | • | 95.0 | 98.0 | 102.0 | 101.0 | 98.0 | 94.0 | 91.0 | 84.0 | 77.0 | 106.8 | 99.9 |
| Area Sources | | | | | | | | | | | | | | | | |
| Const_Dozer_WF | Construction: Bulldozer (Wellfield) | 1 | 118.7 | • | 0 | | 112.4 | 117.4 | 120.4 | 115.4 | 113.4 | 110.4 | 104.4 | 98.4 | 124.0 | 118.7 |
| Const_SS_ISR | Construction: Skid Steer (ISR Plant) | 1 | 105.8 | • | 0 | | 99.5 | 104.5 | 107.5 | 102.5 | 100.5 | 97.5 | 91.5 | 85.5 | 111.1 | 105.8 |
| Const_SS_WF1 | Construction: Skid Steer (Wellfield 1) | 1 | 105.8 | • | 0 | | 99.5 | 104.5 | 107.5 | 102.5 | 100.5 | 97.5 | 91.5 | 85.5 | 111.1 | 105.8 |
| Const_SS_WF2 | Construction: Skid Steer (Wellfield 2) | 1 | 105.8 | • | 0 | | 99.5 | 104.5 | 107.5 | 102.5 | 100.5 | 97.5 | 91.5 | 85.5 | 111.1 | 105.8 |
| Const_Dozer_CWP | Construction: Bulldozer (Clean Waste Pile) | 1 | 118.7 | • | 0 | | 112.4 | 117.4 | 120.4 | 115.4 | 113.4 | 110.4 | 104.4 | 98.4 | 124.0 | 118.7 |
| FP2_Roof | Freeze Plant: Roof (2 Units) ^[2] | 1 | 86.8 | • | 0 | 70.7 | 74.0 | 76.6 | 86.7 | 82.6 | 78.6 | 74.4 | 71.1 | 70.1 | 89.3 | 84.6 |
| FP6_Roof | Freeze Plant: Roof (6 Units) ^[2] | 1 | 91.6 | 0 | • | 75.5 | 78.8 | 81.4 | 91.5 | 87.4 | 83.4 | 79.2 | 75.9 | 74.9 | 94.1 | 89.3 |
| Gen1_Top1 | Generator 1: Enclosure Top ^[2] | 1 | 99.0 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Top2 | Generator 1: Enclosure Top ^[2] | 1 | 94.9 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Top1 | Generator 2: Enclosure Top ^[2] | 1 | 99.0 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Top2 | Generator 2: Enclosure Top ^[2] | 1 | 94.9 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| ISR_Roof | ISR Plant: Process Area Roof ^[2] | 1 | 86.9 | 0 | • | | 82.0 | 82.4 | 81.8 | 83.5 | 84.5 | 84.1 | 83.1 | 76.9 | 91.8 | 90.2 |
| ISR_DRoof | ISR Plant: Dryer/Calciner Area Roof ^[2] | 1 | 88.4 | 0 | • | 90.3 | 87.8 | 89.2 | 88.5 | 91.2 | 91.2 | 91.6 | 90.8 | 83.8 | 99.4 | 97.6 |
| WF_PHR | Wellfield: Pumphouse Roof ^[2] | 1 | 78.4 | 0 | • | | • | | | | | | | | 85.0 | |
| CGen_roof | Camp Generator - roof | 1 | 97.5 | • | • | | | | | | | | | | | |
| OGen_roof | Operations Centre Generator - roof | 1 | 97.5 | • | • | | | | | | | | | | | |
| Vertical Area Sources | | | | | | | | | | | | | | | | |
| FP2_Walls | Freeze Plant: Walls (2 Units) ^[2] | 1 | 86.1 | • | 0 | 70.7 | 74.0 | 76.6 | 86.7 | 82.6 | 78.6 | 74.4 | 71.1 | 70.1 | 89.3 | 84.6 |
| FP6_Walls | Freeze Plant: Walls (6 Units) ^[2] | 1 | 90.9 | • | • | 75.5 | 78.8 | 81.4 | 91.5 | 87.4 | 83.4 | 79.2 | 75.9 | 74.9 | 94.1 | 89.3 |
| Gen1_Intake | Generator 1: Air Intake [2] | 1 | 105.4 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Discharge | Generator 1: Discharge Opening ^[2] | 1 | 120.5 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Side1 | Generator 1: Enclosure Side [2] | 1 | 97.1 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Side2 | Generator 1: Enclosure Side [2] | 1 | 99.4 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |

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| Source ID | Source Description | Number of | Sound | Active S | itatus | | | Octave Ban | d Centre Fre | quency (Hz); | Sound Powe | r Level (dB) | | | Ove | erall |
|----------------|--|-----------|-------------|--------------|------------|-------|-------|------------|--------------|--------------|------------|--------------|-------|-------|-------|-------|
| | | Identical | Power Level | Construction | Operations | 31.5 | 63 | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 | dB | dBA |
| | | Sources | (dBA) | | | | | | | | | | | | | |
| Gen1_Side3 | Generator 1: Enclosure Side [2] | 1 | 97.1 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Side4 | Generator 1: Enclosure Side [2] | 1 | 99.5 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Side5 | Generator 1: Enclosure Side ^[2] | 1 | 96.8 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen1_Side6 | Generator 1: Enclosure Side ^[2] | 1 | 93.5 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Intake | Generator 2: Air Intake ^[2] | 1 | 105.4 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Discharge | Generator 2: Discharge Opening ^[2] | 1 | 120.5 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Side1 | Generator 2: Enclosure Side ^[2] | 1 | 97.1 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Side2 | Generator 2: Enclosure Side ^[2] | 1 | 99.4 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Side3 | Generator 2: Enclosure Side ^[2] | 1 | 97.1 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Side4 | Generator 2: Enclosure Side ^[2] | 1 | 99.5 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Side5 | Generator 2: Enclosure Side ^[2] | 1 | 96.8 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| Gen2_Side6 | Generator 2: Enclosure Side ^[2] | 1 | 93.5 | • | • | 105.2 | 111.0 | 116.5 | 116.5 | 113.8 | 115.8 | 113.8 | 107.0 | 101.0 | 123.0 | 119.9 |
| ISR_PW | ISR Plant: Process Area Walls ^[2] | 1 | 88.5 | 0 | • | | 82.0 | 82.4 | 81.8 | 83.5 | 84.5 | 84.1 | 83.1 | 76.9 | 91.8 | 90.2 |
| ISR_DCW1 | ISR Plant: Dryer/Calciner Area Wall ^[2] | 1 | 87.3 | 0 | • | 90.3 | 87.8 | 89.2 | 88.5 | 91.2 | 91.2 | 91.6 | 90.8 | 83.8 | 99.4 | 97.6 |
| ISR_DCW2 | ISR Plant: Dryer/Calciner Area Wall ^[2] | 1 | 79.0 | 0 | • | 90.3 | 87.8 | 89.2 | 88.5 | 91.2 | 91.2 | 91.6 | 90.8 | 83.8 | 99.4 | 97.6 |
| WF_PHW | Wellfield: Pumphouse Walls ^[2] | 1 | 76.1 | 0 | • | | | | | | | | | | 85.0 | |
| CGen_walls | Camp Generator: Walls | 1 | 102.8 | • | • | | | | | | | | | | | |
| OGen_walls | Operations Centre Generator: Walls | 1 | 102.8 | • | • | | | | | | | | | | | |

Notes:

[1] For the line sources, the octave band sound power data is the unadjusted sound power, while the Lw provided is adjusted for the active time based on the route length and speed of travel.

[2] For area and vertical area sources that represent building envelopes, the octave band data is the interior sound pressure level in the room, and the Lw is the calculated sound power based on the transmission loss of the building and size of the building component.

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